

The Effects of Furnace Configuration Using The Torch High Temperature Combustion Analyzer

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Abstract

In the evaluation of industrial process waters and wastewaters, of particular interest is organic carbon contamination from either microbial or synthetic derivatives, due to their possible environmental impact. High temperature combustion total organic carbon analyzers provide the most efficient way to measure organic carbon in these waters. The furnace parameters for high temperature combustion analyzers dictate the oxidation effectiveness of the sample carbon, which in turn affects the total organic carbon results. This presentation will cover the analytical effects of temperature, catalyst type and combustion tube configuration on total organic carbon analysis.



Introduction

Traditionally, High Temperature Combustion (HTC) analyzers have relied upon furnace temperature and catalyst function to demonstrate the best performance characteristics for the analyzer. Recent advancements have brought pressure, whether low or high, into the discussion of analyzer performance. Regardless of temperature, catalyst type, or pressure setting, the combustion tube has been the center point of all three instrument parameters. As such, its dimensions and dynamics are critical to the analyzer's optimal performance. The combustion tube used in this analysis was a quartz tube packed with alumina based catalyst layered in between two beds of quartz wool. The final strata were a platinum screen held in place by a solid sleeve. The Torch HTC Analyzer, developed by Teledyne Tekmar, uses a new catalyst that is better suited for difficult sample matrices. It is controlled by the user-friendly TekLink[™] software that has predefined instrument methods and numerous programmable parameters. This enables the user to begin sample analysis without delay by employing the preset methods, without losing the flexibility to design custom methods.

| Torch Calibration Matrix | | | | | | | |
|--------------------------------|------|------|------|--|--|--|--|
| 0.50mL Sample Injection Volume | | | | | | | |
| 680°C 720°C 850°C | | | | | | | |
| 50 psig | FC 1 | FC 2 | FC 3 | | | | |
| 30 psig | | | | | | | |

Table 1: Torch calibration analysis comparison matrix. (FC – Furnace Configuration)

Experimental - Instrument Conditions

In this study, the Torch HTC analyzer was configured with three different temperature settings, two different pressure settings and calibrated according to the matrix in Table 1. The general furnace method parameters used to generate all calibration curves are depicted in Table 2. The resulting curves were then compared to show the effects of changing instrument parameters on the analysis. A sample injection volume of 0.5mL was kept constant throughout the experiment.

Torch Analysis Overview

The following steps give a basic description of the TOC Torch methodology for direct TOC analysis:

- 1. <u>Autosampler needle rinse</u>. The syringe pulls deionized water and flushes the autosampler needle into a rinse station at the autosampler.
- 2. <u>Acid addition into the Inorganic Carbon (IC) Sparger Chamber</u>. The syringe pulls sample and dispenses it into the IC Sparger Chamber, followed by the addition of a 20% acid solution to bring the solution to a pH of 2.0 or less.
- 3. <u>IC is sparged from the sample</u>. Carbon dioxide (CO₂) free air or oxygen is sparged through the sample in the IC Sparger Chamber to remove the IC in the sample. For TOC analysis the IC is vented to the atmosphere. For IC analysis it is sent to the detector.
- 4. <u>Furnace Combustion</u>. The sample is added drop-wise into the combustion tube, containing the catalyst, located inside of the furnace. The heat from the furnace oxidizes the carbon into the form of CO₂. This oxidation process is promoted by the catalyst. The CO₂ is sent through the sample pathway into the NDIR detector by the CO₂ free air that is metered by a Mass Flow Controller (MFC).
- 5. <u>Water and halide removal</u>. Before the CO₂ gas reaches the detector, it is sent through two water removal systems, a mist trap and permeation dryer. It is then sent to the halide scrubber to remove any chloride interference.
- 6. <u>NDIR Detection</u>. A valve located at the outlet of the detector prevents the escape of CO₂ from the detector. Once all of the CO₂ is inside the detector, a single measurement is made to determine the amount of CO₂ gas in the detector cell. The reading correlates directly to the concentration of the carbon contribution from the sample.
- 7. <u>Rinse</u>. The syringe pulls in reagent water through the 7-Port Valve and rinses the IC Chamber. This rinse water is then removed prior to the next sample analysis.

TekLink[™] software has programmable parameter settings within the method. The gas flow rates are programmable and metered by the MFC. The use of a MFC to meter the gas flow rates not only allows instantaneous control of system flow but also the delay of gas flow to the furnace after sample introduction. The flexibility of flow control permits the end user to define the amount of time the sample is in contact with the catalyst. This combination of heat, pressure and flow control provides superior precision over flow through cell instruments.

| Parameter | Value |
|---------------------------------|-----------|
| Sample Volume | 0.50mL |
| Water Chase Volume | 1.00mL |
| Dilution | 1:1 |
| Number of Injection Line Rinses | 1 |
| Injection Line Rinse | On |
| Injection Line Rinse Volume | 0.50mL |
| Acid Volume | 0.50mL |
| IC Sparge Flow | 200mL/min |
| Carrier Gas Delay Time | 0.40 min |
| IC Sparge Time | 0.50 min |
| TN Detector Module Enable | Off |
| Detector Sweep Flow | 500mL/min |
| Furnace Sweep Time | 1.00 min |
| System Flow | 500mL/min |

Table 2: Torch instrument method parameters. Parameters highlighted in red were changed during the experiment

| Parameter | Value |
|--------------------------------|-----------|
| Mixer Magnet Enable | Off |
| Sparge In Vial Enable | Off |
| Needle Rinse Volume | 2.5mL |
| Vial Prime Volume | 2.0mL |
| IC Sample Prime Volume | 2.0mL |
| Baseline Stabilize Time | 0.75 min |
| Detector Pressure Flow | 175mL/min |
| Syringe Speed Waste | 10 |
| Syringe Speed Acid | 7 |
| Syringe Speed DI Water | 7 |
| NDIR Pressurization | 50 psig |
| Syringe Speed Sample Dispense | 7 |
| Syringe Speed Sample Aspirate | 7 |
| Syringe Speed IC Dispense | 7 |
| NDIR Pressure Stabilize | 7 |
| Syringe Speed IC Aspirate | 5 |
| NDIR Pressure Stabilize | 0.60 min |
| Sample Mixing | Off |
| Sample Mixing Cycles | 1 |
| Sample Mixing Volume | 2.5 |
| Syringe Speed Furnace Dispense | 3 |
| Syringe Speed Furnace Aspirate | 5 |
| Furnace Temperature | 680°C |

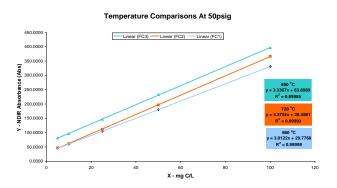


Figure 1: Calibrations compared at three furnace temperature settings with a pressure setting of 50 psig.

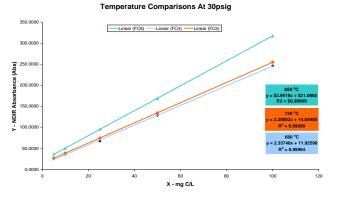
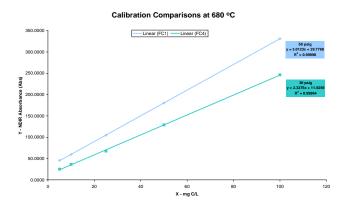
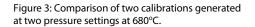


Figure 2: Calibrations compared at three furnace temperature settings with a pressure setting of 30 psig.





| | FC - 1 Checks | | | | | | |
|-----------|--|----------|------------------------|------------|------|--|--|
| | Concentration (ppm) | Dilution | Result | Std. Dev. | RSD | | |
| | 5.0000 | 1:20 | 5.3387 ppm (PASS) | 0.0585 ppm | 1.1% | | |
| | 10.0000 | 1:10 | 9.0280 ppm (PASS) | 0.1166 ppm | 1.3% | | |
| | 25.0000 | 1:4 | 24.5576 ppm (PASS) | 0.2347 ppm | 1.0% | | |
| | 50.0000 | 1:2 | 49.7177 ppm (PASS) | 0.2563 ppm | 0.5% | | |
| | s of Furnace Con | - | 100.8522 ppm (PASS) | 2.7885 ppm | 2.8% | | |
| The Torch | The Torch High Temperature Combustion Analyzer | | | | | | |

Calibration comparisons at 720 °C 400.00 Linear (FC5) Linear (FC2) 350 0000 50 psig y = 3.3752x + 2 R² = 0.999 ice (Abs 250.000 200.00 Ahs NDIR 150.000 100.000 50.0 0.0000 80 X - mg C/L

Figure 4: Comparison of two calibrations generated at two pressure settings at 720°C.

| FC - 4 Checks | | | | |
|--------------------------------|----------|-----------------------|-----------------------------|------|
| Concentration (ppm) | Dilution | Result | Std. Dev. | RSD |
| 5.0000 | 1:20 | 5.4720 ppm (PASS) | 0.1514 ppm | 2.8% |
| 10.0000 | 1:10 | 9.7242 ppm (PASS) | 0.0884 ppm | 0.9% |
| 25.0000 | 1:4 | 26.0439 ppm (PASS) | 0.1712 ppm | 0.7% |
| 50.0000 | 1:2 | 52.5993 ppm (PASS) | 0.8153 ppm | 1.6% |
| Sales/Suppor 4736 Socialvil | | (DAGG) | - 223872000 m 040 | 2.3% |

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| FC - 5 Checks | | | | | |
|------------------------|----------|------------------------|------------|------|--|
| Concentration (ppm) | Dilution | Result | Std. Dev. | RSD | |
| 5.0000 | 1:20 | 5.1197 ppm (PASS) | 0.1837 ppm | 3.6% | |
| 10.0000 | 1:10 | 10.0741 ppm (PASS) | 0.1845 ppm | 1.8% | |
| 25.0000 | 1:4 | 26.5163 ppm (PASS) | 0.4210 ppm | 1.6% | |
| 50.0000 | 1:2 | 52.9563 ppm (PASS) | 0.2969 ppm | 0.6% | |
| 100.0000 | 1:1 | 102.3318 ppm (PASS) | 2.5108 ppm | 2.5% | |

| FC - 2 Checks | | | | | |
|------------------------|----------|-----------------------|------------|------|--|
| Concentration (ppm) | Dilution | Result | Std. Dev. | RSD | |
| 5.0000 | 1:20 | 5.4031 ppm (PASS) | 0.0647 ppm | 1.2% | |
| 10.0000 | 1:10 | 10.3458 ppm (PASS) | 0.5203 ppm | 5.0% | |
| 25.0000 | 1:4 | 25.0892 ppm (PASS) | 0.5596 ppm | 2.2% | |
| 50.0000 | 1:2 | 50.1484 ppm (PASS) | 0.5305 ppm | 1.1% | |
| 100.0000 | 1:1 | 99.8891 ppm (PASS) | 0.5073 ppm | 0.5% | |

Table 3: Comparison of calibration check standard analyses. Each set of check standards were analyzed at 680°C.

Table 4: Comparison of calibration check standard analyses. Each set of check standards were analyzed at 720°C.

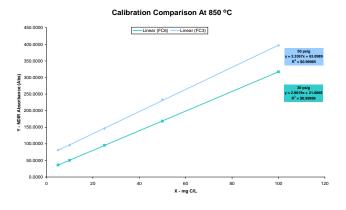


Figure 5: Comparison of two calibrations curves generated at two pressure settings at 850°C.

| FC - 6 Checks | | | | | |
|------------------------|----------|-----------------------|------------|-------|--|
| Concentration (ppm) | Dilution | Result | Std. Dev. | RSD | |
| 5.0000 | 1:20 | 4.8182 ppm (PASS) | 0.1801 ppm | 3.74% | |
| 10.0000 | 1:10 | 10.3289 ppm (PASS) | 0.3536 ppm | 3.42% | |
| 25.0000 | 1:4 | 26.0589 ppm (PASS) | 0.6137 ppm | 2.36% | |
| 50.0000 | 1:2 | 53.2665 ppm (PASS) | 1.7843 ppm | 3.35% | |

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| 100.0000 | 1:1 | 105.6098 ppm | 4.1293 ppm | 3.91% |
|----------|-----|--------------|------------|-------|
| | | (PASS) | | |

| | F | C - 3 Checks | | |
|------------------------|----------|------------------------|------------|-------|
| Concentration (ppm) | Dilution | Result | Std. Dev. | RSD |
| 5.0000 | 1:20 | 5.3387 ppm (PASS) | 0.0585 ppm | 1.10% |
| 10.0000 | 1:10 | 9.0280 ppm (PASS) | 0.1166 ppm | 1.29% |
| 25.0000 | 1:4 | 24.5576 ppm (PASS) | 0.2347 ppm | 0.96% |
| 50.0000 | 1:2 | 49.7177 ppm (PASS) | 0.2563 ppm | 0.52% |
| 100.0000 | 1:1 | 100.8522 ppm (PASS) | 2.7885 ppm | 2.76% |

Table 5: Comparison of calibration check standard analyses. Each set of check standards were analyzed at 850°C.

Benefits/Conclusion

The calibration curve efficiency, for each pair of curves, was evaluated through analyzing the same points of the calibration curves as check standards using the automated dilution feature of the TekLink[™] software. The Torch HTC system performed very well on all calibration curves for linearity and precision as indicated in Tables 3-5. A comparison of the calibration curves in Figures 1 and 2 demonstrates that regardless of pressure settings, an increase in temperature results in an increase of background, but this does not significantly affect linearity or precision. The new Torch HTC Analyzer has a combined instrument and autosampler platform, user friendly TekLink[™] software, and Static Pressure Concentration (SPC) technology (patent pending). All of these features combined demonstrate Teledyne Tekmar's continuous leadership in instrument manufacturing.